Depleted Uranium as Aggregate in Concrete Shielding Material

Les Dole

Oak Ridge National Laboratory, P.O. Box 2008: Oak Ridge, TN 37831-6273 Phone: (865) 576-4310; E-mail: <u>dolelr@ornl.gov</u>

Presented at the

Russian-American Workshop on Management of Depleted Uranium December 9-10, 2002, Moscow, Russia

U.S. Department of Energy, Russian Academy of Science, State Unitary Enterprise, and Russian Research Institute of Chemical Technology

*Managed by UT-Battelle, LLC, for the U.S. Department of Energy under contract DE-AC05-00OR22725. The submitted manuscript has been authored by a contractor of the U.S. Government under contract DE-AC05-00OR22725. Accordingly, the U.S. Government retains a nonexclusive, royalty-free license to publish or reproduce the published form of this contribution, or allow others to do so, for U.S. Government purposes.



Conclusions

- Combinations of gamma-absorbing depleted uranium (DU) and neutron-absorbing hydrated binders are shown to effectively reduce the size and weight of storage, transport, and disposal casks
- DUCRETE[™] will become one of the materials of choice for advanced spent nuclear fuel (SNF) casks
 - Requires the demonstration of low-cost fabrication processes
 - Requires the demonstration of long-term durability under expected service conditions

TM = trademark, patented technology OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



Presentation Outline

- Programmatic background
- Description of technology
- Summary of previous accomplishments
- Description of current studies and results
- Conclusions



Vision and Mission of the DU Uses R&D Project

Reduce DU disposition costs

 Consume the inventory of DU by using it in nuclear shielding applications

 Bring advanced DU shielding technologies to the level of demonstrated technical success and readiness for full-scale deployment



Use of DU Offers Advantages in SNF Storage, Transport, and Disposal Casks

- Concrete with DU (DUCRETE[™]) can be used in current cask designs, such as the <u>con</u>crete <u>stor</u>age (CONSTOR) cask that is to be used for RBMK fuels
- Cermets can also be used in DU-steel modification to baskets
 - Addition of neutron absorbers
 - Addition of DUO₂ basket fill



Composition of DUCRETE[™] – <u>D</u>epleted <u>Uranium</u> con<u>CRETE</u>

- Coarse-graded sintered UO₂ aggregates at a density of >8.9 g/cm³
- Cementitious binder, similar to Portland cement
- Fine aggregates, like quartz, fly ash, microreinforcement, and/or colemanite sands
- Water



DUCRETE[™] Combines the High Density of DU with Binders of Low-Z Elements to Optimize Gamma and Neutron Attenuation





Comparison of wall thicknesses required to attenuate to 10 mR/H the neutron and gamma doses from 24 pressurized-water-reactor spent fuel assemblies



DUCRETE[™] Storage Casks are Considerably Smaller and Lighter than Casks Constructed of Ordinary Concrete



JT-BATTELI

8

U. S. DEPARTMENT OF ENERGY

DUAGG[™] Briquettes are Stabilized DU Aggregates with Basalt Sintering Agent



Briquettes are pressed, solidified by liquid-phase sintering, and then crushed and gap graded for use in high-strength DUCRETE[™] at 5000 to 6000 psi, (35–42 MPa)





DUAGG[™] Processing and Sizing



U. S. DEPARTMENT OF ENERGY

Substituting DUCRETE[™] in CONSTOR Cask Increases Capacity and Protection

- Reduces size and weight
- Allows higher thermal loads
- Meets criteria for improved technical and economic performance
- Allows enhanced physical protection within current weight limits
- Complies with emerging regulatory requirements and standards





DUCRETE[™] Reduces CONSTOR Shielding to 11.5 in. and Increases Thermal Capacity by 1.5

	Sierr	a System	DL	JCRETE Sys	tem	GI		R
Cask Dimensions	Inside Steel Shell	Concrete	Inside Steel Shell	DUCRETE	Outside Steel Shell	Inside Steel Shell	Heavy Concrete	Outside Steel Shell
Thickness (in.)	1.75	29.00	1.00	11.50	1.00	1.57	17.40	1.57
ID (in.)	70.50	74.00	70.5	72.50	95.5	70.5	73.65	108.4
OD (in.)	74.0	132.0	72.5	95.5	97.5	73.6	108.4	111.6
Inside Length (ft)	15.0	15.0	15.0	15.0	15.0	15.0	15.0	15.0
Wall cross section (ft ²)	2.8	65.2	1.6	21.1	2.1	2.5	34.6	3.8
Wall Volume (ft ³)	41.4	977.5	23.4	316.1	31.6	37.1	518.5	56.7
End Thickness (in.)	1.75	11.6	1.00	4.6	1.00	1.57	7.0	1.57
End (2) Volume (ft ³)	27.7	183.7	8.6	38.1	8.6	17.8	74.4	17.8
Total Volume (ft ³)	69.1	1161.2	32.0	354.3	40.2	55.0	592.9	74.5
Density (lb/ft ³)	491	146	491	362	491	491	207	491
Mass (lb)	33,926	169,684	15,732	128,414	19,749	26,992	122,993	36,594
Component Mass (ton)	17.0	84.8	7.9	64.2	9.9	13.5	61.5	18.3
Container Mass (ton)		102		82			93	
Container Weight Reduction				-20%			-8%	
Shielding Equivalency (lb/ft2)	72	353	41	347	41	64	301	64
Total Shielding Equivalency		425			429			430



Theoretical Thermal Conductivities of Composites Used in Calculations

Concrete	Volume Percent of Component			Thermal Conductivity, W/(m•K)		
	Cement Paste	Steel	Lime- stone	Barium Sulfate	UO ₂ Powder	
Normal Concrete	0.25	0.10	0.65			2.9
Heavy Concrete	0.25	0.10		0.65		3.4
DUCRETE	0.25	0.12			0.63	7.0



Several DUCRETE[™] Demonstration Programs Have Been Successfully Completed



Test block sectioned after curing



30-gal-drum overpack

OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



Conceptual Designs of DUCRETE[™] Casks Have Been Developed by Duke Power for HLW Storage

Shielding Effectiveness vs Wall Thickness

DUCRETE TM Thickness (in.)	Surface Dose Rate (mrem/h)	Dose Rate @ 2 (mrem/h)
10	41	10
11	27	6
12	19	4
13	15	3
14	12	2
15	9	2
16	8	1

OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY

DUCRETE Overpack System





Current DUCRETE™ Technology Development

- DUAGG[™] manufacturing process optimization, cost reduction, and demonstration
- Material properties characterization for matrix and aggregate stability with aging under service conditions
- Optimized binder and DUAGG[™] for gamma and neutrons for specific cask designs
- Fabrication and testing of full-scale cask prototypes under a cooperative research and development agreement (CRADA)



Current Laboratory Studies

OAK RIDGE NATIONAL LABORATORY **U. S. DEPARTMENT OF ENERGY**



Current DUAGG[™] Exposure Studies Using ASTM C289-94 Standard Test Method

- At a constant surface-to-liquid ratio of 1:10, the sintered DUAGG[™] samples are exposed to
 - distilled (DI) water
 - 1 N sodium hydroxide (NaOH) standard solution
 - saturated water extract of high-alkali cement
- The three exposure temperatures and six time intervals are 25, 66, and 150°C at intervals of 30, 60, 90, 180, 240, and 360 days



Unexposed DUAGG[™]



Particle A contains Al Particle B contains Ti and some Mg Area C contains the round DU particles surrounded by the basalt phase



Uranium Leached from DUAGG[™]





DUAGG[™] Exposed to Cement Water for 6 Months at 150°C





DUAGG Exposed to 1 NNaOH for 6 months at 150°C



Alkali reaction products with Na, Al, Si, Ca, and Ti

OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



Proposed CRADA Between ORNL and the U.S. GNSI for the Development of Advanced Spent Nuclear Fuel Storage, Transport, and Disposal Casks and Overpacks

CRADA = Cooperative Research and Development Agreement; GNSI = General Nuclear Services, Inc. OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY

Conclusions

- Combinations of gamma-absorbing DU and neutronabsorbing hydrated binders are shown to effectively reduce the size and weight of storage, transport, and disposal casks
- DUCRETE[™] will become one of the materials of choice for advanced spent nuclear fuel (SNF) casks
 - Requires the demonstration of low-cost fabrication processes
 - Requires the demonstration of long-term durability under expected service conditions



Additional Material for Discussion

OAK RIDGE NATIONAL LABORATORY U. S. Department of Energy



Summary

- DUCRETE[™] casks have
 - Smaller dimensions
 - Lighter weight
 - Higher SNF heat loading
 - Potentially greater physical protection against assault
- We are conducting laboratory experiments to characterize DUAGG[™]/DUCRETE[™] materials
- We are conducting preliminary cost studies
- We are pursuing a collaboration with GNSI to design and demonstrate the next generation of SNF casks



Thermal Conductivities of DUCRETE™ Components Used in Calculations

Material	Thermal Conductivity, W/(m•K)		
Iron	84.3		
Stainless Steel	16.0*		
Cement Paste	2.96*		
Limestone	0.94*		
Barium Sulfate	2.51 *		
UO ₂ (Solid)	8.37		
UO ₂ (Powder, 68 vol %)	6.93*		

*Used in subsequent calculations OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



Aluminum Leached from DUAGG[™]





Silicon Leached from DUAGG[™]



OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



GNB CONSTOR Cask for RMBK SNF







Estimated Need for DUO₂

Purpose	Amount, tonnes	Time, years
Lab scale tests	2–5	Now
Intermediate-scale tests	5–10	1–2
Pilot-scale cask fabrication	18–22	2–3
Full-scale cask fabrication	210–240	3–5
Total	380–440	7–11

Potential costs \$1.5M-\$30M (current commercial)



Preliminary Plant Design Study for the Production of DUAGG[™]



Objective and Scope

- Conceptual design for DUAGG[™] plant to estimate potential capital and operating costs
- Design of a DUAGG[™] plant that receives DUO₂; presses and sintered briquettes; and crushes, sizes, and packages DUAGG[™] to be used in highstrength DUCRETE[™] for SNF casks



Baseline Assumptions for Scaling the Plant and Equipment

- Achieve production rate of 2834 tonnes per year to meet 30% penetration of domestic market for SNF storage and transport casks (about 50 casks)
- Receive DUO₂ from external source
- Receive sintering and binding materials for milling, blending, pressing, sintering, and crushing
- Produce crushed, gap-graded, and amended DUAGG[™] product for use in DUCRETE[™] that is formed off-site





OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



Process Unit Operations



OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY



Preliminary Capital Cost Elements

	Capital Costs (\$1,000 USD)
Civil/Site Preparation	500
Utilities Building Services	56
Building Structures	2,620
Process Equipment	2,224
Special Process Services	35
Engineering	1,591
Piping	1,204



Preliminary Capital Cost Elements (cont.)

	Capital Costs (\$1,000 USD)
Installation Labor	1,205
Electrical	220
Spare Parts	346
Management	1,000
Safety Systems	600
Shipping	110
Total Capital Investment	11,601



Preliminary Total Operating Cost

Baseline Cost of DUO₂: \$0 USD/ton

	\$1,000 USD/year	Capital Recovery
Labor	4,014	34 5%
Electricity	56	J.1.7/0
Chemicals	309	Chemi
Cost of DUO ₂	0	4.59
Capital Recovery	2,320	Elec
Total Operating Cost	6,699	,



OAK RIDGE NATIONAL LABORATORY U. S. DEPARTMENT OF ENERGY UT-BATTELLE

Future Engineering Analyses

- Determine the specification of DUO₂ feed to plant
- Simplify the grinding, mixing, and sintering processes to reduce labor required
- Optimize briquetting and final grinding processes
- Examine other agglomeration processes
- Conduct a parametric process parameters study on the reproducibility of DUAGG[™]
- Research microreinforcement in the DUCRETE™



Russian RBMK Spent Fuel Cask with Heavy Concrete





Heavy concrete with steel shot and barium sulfate

41

GNB CONSTOR test cask for RBMK SNF

